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## REISSUE PATENT APPLICATION TRANSMITTAL

Docket No. : 36912/CM/S61  
 Inventor(s) : Dah-Ben Liang, Alysia C. White, Zhigang Fang, Jiinjen Albert Sue  
 Original Patent Number : 5,791,422  
 Original Patent Issue Date : August 11, 1998  
 (Month/Day/Year)  
 Title : Rock Bit with Hardfacing Material Incorporating Spherical Cast Carbide Particles  
 Express Mail Label No. : EL521383879US

**ADDRESS TO:** Box Reissue  
 Assistant Commissioner for Patents  
 Washington, D.C. 20231

Date: August 10, 2000

## APPLICATION FOR REISSUE OF UTILITY PATENT

## 1. Application Elements

- ☒ Fee Transmittal Form (*Submit an original and a duplicate for fee processing*)  
☒ Specification and Claims  
☒ Reissue Declaration (*37 CFR 1.175*)  
☒ Drawing(s) (proposed amendments, if appropriate)

## 2. Original U.S. Patent

- ☒ Offer to Surrender Original Patent (*37 CFR 1.178*)  
☒ Ribbonded Original Patent Grant  
☐ Affidavit/Declaration of Loss  
☐ Title Report  
☐ Enclosed  
☐ Request and fee (*37 CFR § 1.19(b)(4)*)

## 3. Original U.S. Patent currently assigned?

- ☒ Yes ☐ No  
 (If Yes, check applicable box(es))  
☒ Written Consent of all Assignees  
☒ 37 CFR 3.73(b) Statement

## 4. Accompanying Application Parts

- ☒ Power of Attorney  
☒ Transfer drawings from Patent File  
☐ Foreign Priority Claim (*35 USC 119*)(if applicable)  
☐ English Translation of Reissue Oath/Declaration (if applicable)  
☒ Information Disclosure Statement (IDS)/PTO-1449  
☐ 10 Copies of IDS citations  
☐ Small Entity Statement(s)  
☐ Statement filed in prior application, status still proper and desired  
☒ Return Receipt Postcard (MPEP 503) (Should be specifically itemized)  
☒ Other Copy of Recorded Assignment

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REISSUE PATENT APPLICATION TRANSMITTAL

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Docket No.: 36912/CM/S61

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5. CORRESPONDENCE ADDRESS

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Respectfully submitted,

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CM/mac

United States Patent [19]  
Liang et al.

[54] **ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES**

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[21] **Appl. No.:** 815,745

[22] **Filed:** Mar. 12, 1997

**Related U.S. Application Data**

[60] **Provisional application No.** 60/014,225, Mar. 27, 1996, and  
provisional application No. 60/014,731, Mar. 12, 1996.

[51] **Int. Cl.<sup>6</sup>** ..... E21B 10/00

[52] **U.S. Cl.** ..... 175/374; 175/425; 428/539.5

[58] **Field of Search** ..... 175/331, 374,  
175/432, 425; 428/539.5

[56] **References Cited**

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*Primary Examiner*—Roger J. Schoepfel  
*Attorney, Agent, or Firm*—Christie, Parker & Hale, LLP

[57] **ABSTRACT**

An improved hardfacing for teeth and other surfaces of milled tooth rock bits includes steel in the range of from 20 to 50 percent by weight, and filler in the range of from 50 to 80 percent by weight. The filler includes spherical cast tungsten carbide particles alone or in a mixture of other tungsten carbide particles such as crushed cast spherical or crushed cemented tungsten carbide, macrocrystalline tungsten carbide, or the like. The single crystal monotungsten tungsten carbide particles have a particle size in the range of from 16 to 40 mesh and/or in the range of from 80 to 200 mesh.

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**ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES**

**CROSS-REFERENCE TO RELATED  
APPLICATIONS**

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This application claims the benefit of provisional patent applications Ser. Nos. 60/014,731, filed Mar. 12, 1996, and 60/014,225, filed Mar. 27, 1996.

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**FIELD OF THE INVENTION**

This invention relates to improved fracture- and wear-resistant hardfacing compositions applied to wear surfaces on teeth on bits for drilling oil wells or the like.

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**BACKGROUND OF THE INVENTION**

Bits for drilling oil wells and the like commonly have a steel body which is connected at the bottom of a drill string. Steel cutter cones are mounted on the body for rotation and engagement with the bottom of a hole being drilled to crush, gouge, and scrape rock for drilling the well. One important type of rock bit referred to as a milled tooth bit has roughly triangular teeth protruding from the surface of the cone for engaging the rock. The principal faces of such a milled tooth that engage the rock are usually dressed with a layer of hardfacing material to resist wear. The specific tooth geometry forms no part of this invention.

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Conventional hardfacing usually comprises particles of tungsten carbide bonded to the steel teeth by a metal alloy. In effect, the carbide particles are embedded in a matrix of metal forming a layer on the surface. Most hardfacing on rock bits employs steel alloys containing nickel and cobalt as the matrix, although other alloys may also be used.

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It is quite common in referring to the particulate material in the hardfacing merely as "carbide" without characterizing it as tungsten carbide. The metal carbide principally used in hardfacing is tungsten carbide. Small amounts of tantalum carbide and titanium carbide may be present, although considered to be deleterious. It will be understood that as used herein, reference merely to "carbide" means tungsten carbide.

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Three types of tungsten carbide have been employed for hardfacing. Possibly the most common is crushed cast carbide. Tungsten forms two carbides, WC and W<sub>2</sub>C and there can be an essentially continuous range of compositions therebetween. Cast carbide is typically a eutectic mixture of the WC and W<sub>2</sub>C compounds, and as such is substoichiometric, that is, it has less carbon than the more desirable WC form. Cast carbide is solidified from the molten state and comminuted to the desired particle size.

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Another type of tungsten carbide is so-called macrocrystalline tungsten carbide. This material is essentially stoichiometric WC in the form of single crystals. Most of the macrocrystalline tungsten carbide is in the form of single crystals but some bicrystals of WC may form in larger particles.

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The third type of tungsten carbide used in hardfacing comprises cemented tungsten carbide, sometimes referred to as sintered tungsten carbide. Cemented tungsten carbide comprises small particles of tungsten carbide (e.g., 1 to 15 microns) bonded together with cobalt. Cemented tungsten carbide is made by mixing tungsten carbide and cobalt powders, pressing the mixed powders to form a green compact, and "sintering" the composite at temperatures near the melting point of cobalt. The resulting dense cemented

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carbide can then be comminuted to form particles of cemented tungsten carbide for use in hardfacing.

A typical technique for applying hardfacing to the teeth on a rock bit is by oxyacetylene welding. A welding "rod" or stick is formed of a tube of mild steel sheet enclosing a filler which is primarily carbide particles. The filler may also include deoxidizer for the steel, flux, and a resin binder to retain the particles in the tube during welding. The hardfacing is applied by melting the rod on the face of the tooth. The steel tube melts to weld to the steel tooth and provides the matrix for the carbide particles in the hardfacing. The deoxidizer alloys with the mild steel of the tube.

Although mild steel sheet is used when forming the tubes, the steel in the hardfacing as applied to a rock bit is a hard, wear resistant, alloy steel. This occurs by the dissolution of tungsten, carbon, and possibly cobalt, into the alloy steel from the tungsten carbide during welding. There may also be some mixing with the alloy steel from the teeth on the cone.

It is important to provide as much wear resistance as possible on the teeth of a rock bit cutter cone. The effective life of the cone is enhanced as wear and fracture resistance of the hardfacing is increased. It is desirable to keep the teeth protruding as far as possible from the body of the cone since the rate of penetration of the bit into the rock formation is enhanced by longer teeth (however, unlimited length is infeasible since teeth may break if too long for a given rock formation). As wear occurs on the teeth, they get shorter and the drill bit may be replaced when the rate of penetration decreases to an unacceptable level. It is desirable to minimize wear so that the footage drilled by each bit is maximized. This not only decreases direct cost, but also decreases the frequency of having to "round trip" a drill string to replace a worn bit with a new one.

U.S. Pat. No. 4,944,774 discloses a hardfacing material for use with the teeth of rock bits that comprises a mixture of crushed cemented tungsten carbide having a particle size in the range of from 20-30 mesh, and macrocrystalline tungsten carbide having a particle size in the range of from 40-80 mesh. Such a hardfacing material is known to provide a good degree of wear resistance and abrasion protection of the inner teeth, and somewhat improved wear resistance of the gage surfaces of the cone and gage row of teeth.

Advances in wear resistance of hardfacing on the teeth and gage surfaces of the cone are desirable to increase the duration during which a hole diameter can be maintained, to enhance the footage a drill bit can drill before becoming dull, and to enhance the rate of penetration of such drill bits. Such improvements translate directly into reduction of drilling expense.

#### BRIEF SUMMARY OF THE INVENTION

There is, therefore, provided in practice of this invention according to a presently preferred embodiment, a hardfacing material for both an inner row of rock bit teeth, and gage surfaces of a rock bit cone and gage row of rock bit teeth. The hardfacing material includes spherical cast carbide particles alone or in a mixture including other carbide particles such as spherical or crushed cemented carbide, macrocrystalline carbide, carburized carbide, or the like. The carbide particles are in a matrix of alloy steel welded to the steel of the teeth of the cutter cone.

#### BRIEF DESCRIPTION OF THE DRAWINGS

These and other features and advantages of the present invention will be appreciated as the same becomes better

FIG. 2 is a fragmentary cross section of an exemplary tooth on such a rock bit.

### DETAILED DESCRIPTION

An exemplary milled tooth rock bit comprises a stout steel body 10 having a threaded pin 11 at one end for connection to a conventional drill string. At the opposite end of the body there are three cutter cones 12 for drilling rock for forming an oil well or the like. Each of the cutter cones is rotatably mounted on a pin (hidden) extending diagonally inwardly on one of the three legs 13 extending downwardly from the body of the rock bit. As the rock bit is rotated by the drill string to which it is attached, the cutter cones effectively roll on the bottom of the hole being drilled. The cones are shaped and mounted so that as they roll, teeth 14 on the cones gouge, chip, crush, abrade, and/or erode the rock at the bottom of the hole. The teeth 14G in the row around the heel of the cone are referred to as the gage row teeth. They engage the bottom of the hole being drilled near its perimeter on "gage." Fluid nozzles 15 direct drilling mud into the hole to carry away the particles of rock created by the drilling.

Such a rock bit is conventional and merely typical of various arrangements that may be employed in a rock bit. For example, most rock bits are of the three cone variety illustrated. However, one, two and four cone bits are also known. The arrangement of teeth on the cones is just one of many possible variations. In fact, it is typical that the teeth on the three cones on a rock bit differ from each other so that different portions of the bottom of the hole are engaged by the three cutter cones so that collectively the entire bottom of the hole is drilled. A broad variety of tooth and cone geometries are known and do not form a specific part of this invention.

Exemplary teeth on such a cone are generally triangular in a cross-section taken in a radial plane of the cone. Such a tooth has a leading flank 16 and trailing flank 17 meeting in an elongated crest 18. The flanks of the teeth are covered with a hardfacing layer 19. Sometimes only the leading face of each tooth is covered with a hardfacing layer so that differential erosion between the wear-resistant hardfacing on the front flank of a tooth and the less wear-resistant steel on the trailing face of the tooth tends to keep the crest of the tooth relatively sharp for enhanced penetration of the rock being drilled.

The leading face of the tooth is the face that tends to bear against the undrilled rock as the rock bit is rotated in the hole. Because of the various cone angles of teeth on a cutter cone relative to the angle of the pin on which the cone is mounted, the leading flank on the teeth in one row on the same cone may face in the direction of rotation of the bit, whereas the leading flank on teeth in another row may on the same cone face away from the direction of rotation of the bit. In other cases, particularly near the axis of the bit, neither flank can be uniformly regarded as the leading flank and both flanks may be provided with a hardfacing.

There are also times when the ends of a tooth, that is, the portions facing in more or less an axial direction on the cone, are also provided with a layer of hardfacing. This is particularly true on the so-called gage surface of the bit which is virtually always provided with a hardfacing. The gage surface is a generally conical surface at the heel of a cone

The shape of the carbide particles has been found to affect their toughness. Both cemented carbide and cast carbide

Spherical cast carbide particles have been found to be very tough and hard, testing up to 3000 Hardness Vickers. Processes for producing spherical cast carbide particles are described in U.S. Pat. Nos. 4,723,996 and 5,089,182, which are herein incorporated by reference. Basically, a mixture of tungsten and carbon is heated above its melting point into a constantly flowing stream which is poured onto a rotating cooling surface, typically a water-cooled casting cone, pipe, or concave turntable. The molten stream is rapidly cooled on the rotating surface and forms spherical particles of eutectic tungsten carbide.

Carbide particles are often measured in a range of mesh sizes, for example 40 to 80 mesh. The term "mesh" actual refers to the size of the wire mesh used to screen the carbide particles. For example, "40 mesh" indicates a wire mesh screen with forty holes per linear inch, where the holes are defined by the crisscrossing strands of wire in the mesh. The hole size is determined by the number of meshes per inch and the wire size. The mesh sizes referred to herein are standard U.S. mesh sizes. A standard 40 mesh screen has holes such that only particles having a dimension less than 420  $\mu\text{m}$  can pass. Particles having a size larger than 420  $\mu\text{m}$  are retained on a 40 mesh screen and particles smaller than 420  $\mu\text{m}$  pass through the screen. Therefore, the range of sizes of the carbide particles in a filler is defined by the largest and smallest grade of mesh used to screen the particles. An exemplary filler comprising carbide particles in the range of from 16 to 40 mesh will only contain particles larger than 420  $\mu\text{m}$  and smaller than 1190  $\mu\text{m}$ , whereas another filler comprising particles in the range of from 40 to 80 mesh will only contain particles larger than 180  $\mu\text{m}$  and smaller than 420  $\mu\text{m}$ . Hence, there is no overlap in terms of particle size between these two ranges.

In addition to the carbide in the filler in the tube, it is desirable to include up to five percent by weight of deoxidizer and a temporary resin binder. A suitable deoxidizer is silicomanganese obtained from Chemalloy in Pennsylvania. The nominal composition of the silicomanganese is 65% to 68% manganese, 15% to 18% silicon, a maximum of 2% carbon, a maximum of 0.05% sulfur, a maximum of 0.35% phosphorus, and a balance of iron. Preferably about four percent deoxidizer is used. A small amount of thermoset resin is desirable for partially holding the particles together in the tube so that they do not simply fall out during welding. A half percent by weight of resin is adequate.

The proportion of filler to the weight of the steel tube within which it is enclosed in an exemplary embodiment is 50% to 80% filler and 20% to 50% tube. A presently preferred proportion is in the range of 65% to 75% filler and 25% to 35% tube. These proportions can vary by plus or minus 2%. In order to obtain a weight ratio of filler to steel of 70:30, a  $\frac{5}{32}$  inch (4 mm) diameter tube is made with steel



having a wall thickness of 0.017 inch (0.43 mm). Roughly the same proportions are obtained in a  $\frac{3}{16}$  inch (4.5 mm) diameter steel tube by making it with a wall 0.02 inch (0.5 mm) thick.

According to a presently preferred embodiment, the tungsten carbide portion of the filler comprises spherical cast tungsten carbide in the range of from 10 to 100 percent by weight, with the remainder consisting of the other types of tungsten carbide particles described above. The spherical tungsten carbide particles are in the preferred size ranges of between 16 to 40 mesh and/or between 80 to 200 mesh, however 100 to 200 mesh is preferred in this finer particle size range. For example, a typical filler composition can be made up using 30 kg of 16 to 30 mesh spherical cast tungsten carbide, 40 kg of 16 to 30 mesh crushed cemented tungsten carbide, 25 kg of 40 to 80 mesh macrocrystalline carbide, 4 kg of silico-manganese deoxidizer, and 0.5 kg of phenolic resin binder. The particles are coated with the resin suspended in an alcohol solution which is then dried. After the tubes are loaded with the filler and the ends crimped, the ends are dipped in a solution of phenolic resin in alcohol to add some binder at the ends. The binder is then heat cured to temporarily bind the particles together.

It has been found that the metal matrix may be strengthened by uniformly dispersing ultra-fine carbide particles in the steel matrix without sacrificing toughness. The ultra-fine particles may be a carbide, such as chromium, vanadium or niobium carbide, or a boride such as chromium boride. As used herein, the term "ultra-fine" is defined with respect to the particle size of distinct carbide particles incorporated in the metal matrix as practiced in the prior art, as opposed to carbide particles incorporated in larger carbide particles, such as in cemented tungsten carbide particles as described above. The hypothesized mechanism for this strengthening is dispersion strengthening of the steel matrix. As a result, the wear resistance of the steel matrix is increased and the overall chipping resistance is markedly improved. The ultra-fine carbide particles to be dispersed in the steel matrix according to alternate preferred embodiments of the present invention may be either macrocrystalline tungsten carbide particles, which are crushed and may then be milled for very fine sizes, e.g., below 10  $\mu\text{m}$ , or the ultra-fine particles may be formed by a process in which very small tungsten particles, e.g., 1–50  $\mu\text{m}$ , are carburized to produce a type of tungsten carbide powder generally referred to as carburized carbide. The shape of the ultra-fine carbide particles may be angular or spherical as spherical cast tungsten carbide particles in this preferred size range may also be used for the ultra-fine particles. In a presently preferred embodiment, the ultra-fine particles are included in the hardfacing as a carburized carbide powder containing tungsten carbide particles in the range of from about 15 to 50  $\mu\text{m}$ . A suitable powder containing ultra-fine carbide particles is available from H.C. Stark as MAS-3000 powder. The ultra-fine carbide particles may be introduced directly into the matrix by mixing them with the other carbide particles in the tube rod to be welded. Alternatively, the ultra-fine particles may be uniformly distributed in the matrix by sufficiently overheating the tube rod during welding to induce dispersion of the ultra-fine particles which comprise the cemented carbide particles, causing them to migrate through the matrix by convection.

Presently preferred alternate ratios are provided in the following table:

Exam- ple	Spherical Cemented Carbide (wt %)		Spherical Cast Carbide (wt %)	Ultra- fine Carbide (wt %)	Wt % of the filled-in
	28-35 mesh	48-200 mesh	100-200 mesh	30 $\mu$ m	tube rod
1	70	—	20	10	64
2	—	35	45	20	64
3	40	—	50	10	70

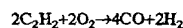
The weight percent of the filled-in tube rod in the above chart may include up to 4% fluxing agent and deoxidizer.

The hardfacing material is applied to the faces of a tooth by heating the face to a welding temperature by an oxy-acetylene or atomic hydrogen torch. When a suitable temperature is reached, the above-described tubular welding "rod" is melted onto the face of the tooth. In an exemplary embodiment, the thickness of the hardfacing layer is about  $\frac{1}{16}$  to  $\frac{3}{32}$  inch (1.6 to 2.4 mm). Dissolution of the silicon-manganese in the mild steel of the tube, possible dissolution of some of the tungsten, carbon, and cobalt of the carbides, and mixing of metal from the body of the cutter cone results in an alloy steel matrix for the carbide particles. Microscopic examination after the cutter cone is carburized, quenched, and tempered indicates a Martensitic phase transformation in the alloy steel matrix of the hardfacing.

During drilling, microcracks frequently initiate in the region of the weld joint, in particular at sharp corners which are high stress regions. The welding sequence is a critical parameter for reducing the formation of microcracks in the hardfacing. The critical surfaces, i.e., those surfaces which experience high compressive stresses during drilling, should be hard faced first, followed by less critical surfaces. Furthermore, the edge of the weld joint of hardfacing should be formed at a low stress region to reduce microcracking. Accordingly, the preferred welding sequence of a drilling tooth is the following: crest and leading flank; trailing flank; and side faces of the tooth. In addition, the weld deposits on a given surface of the tooth should be rolled over the corner to the adjacent surface by at least  $\frac{1}{8}$  inch (3 mm) so that the weld joint is located in the low stress region rather than a sharp edge.

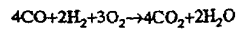
It is hypothesized that the presence of eta phase and oxide particles in the matrix formed as a by-product of the welding process reduces the toughness of the matrix. Eta phase and oxide particles form in the steel matrix during welding due to the presence of excessive oxygen in the torch flame. The eta phase particles, e.g.,  $W_3Fe_3C$  and  $W_3Co_3C$ , are the result of carbon depletion of the tungsten carbide as it reacts with the metals in the matrix. Oxide particles form when the metal alloy in the tube rod reacts with the carbide particles and the oxygen in the oxyacetylene torch flame or from the air surrounding the flame. The eta phase and oxides are brittle compounds. Thus a matrix containing a large portion of eta phase and oxide particles tends to be brittle and more prone to fracture. It has been found that the formation of eta phase and oxide particles in the steel matrix can be minimized by controlling the welding parameters when applying the hardfacing.

An oxyacetylene torch flame has inner, intermediate and outer flame cones. Combustion of acetylene occurs in two stages. The first stage:



uses the oxygen and acetylene supplied from the cylinder. The oxygen-acetylene mixture is achieved and controlled in

the torch. This reaction can be seen as the small inner cone of the flame. The highest temperature is at the point of this cone. The second stage:



uses oxygen supplied from the air surrounding the flame. This combustion zone constitutes the outer blue envelope of the flame. Intermediate between the inner and outer cones there is a non-luminous intermediate cone. When the acetylene/oxygen ratio is about 1 to 1 and there is neither excess oxygen nor acetylene at the tip of the inner cone, the intermediate cone of the flame is regarded as neutral, i.e. neither oxidizing nor carburizing. A short pale green "feather" at the tip of the inner cone is an indication of an excess of acetylene. When the feather is less than about half the length of the inner cone, the flame is regarded as reducing. A longer intermediate flame is considered carburizing.

A neutral flame showing only three cones without a feather or only a very short feather less than about  $\frac{1}{8}$  the length of the inner cone is preferred for welding hardfacing on the teeth of a rock bit cutter cone. The oxygen concentration within the intermediate cone in a neutral flame is quite low and oxides should not be formed when the molten metal is within the outer cone and outside the inner cone. A torch configuration to yield a pointed inner cone is preferred over a configuration that yields a bulbous cone.

Previously, when welding the hardfacing material onto a rock bit, the ratio of lengths of the inner and intermediate flame cones is typically maintained at about 3:1, with the end of the tube rod maintained in a region between the tips of these two flame cones, most likely near the tip of the inner cone since that is the location of the highest temperatures. Welders prefer to hold the tip of the inner cone near the workpiece since welding is faster. A flame ratio of about 3:1 is specified in welding handbooks.

According to a presently preferred method for welding hardfacing onto the teeth of a cutter cone, the inner to intermediate flame cone length ratio is maintained at about 4:1 and the tube rod is maintained in a preferred region of the intermediate flame cone away from the tip of the inner cone between about  $1\frac{1}{2}$  and 3 times the length of the inner cone. Hardfacing is welded onto rock bit cones using various torch tip sizes. For example, Victor welding torches, manufactured by the Thermadyne Company, have a number 6 and a number 7 size torch tip with orifice diameters of 0.27 cm and 0.32 cm, respectively. With a number 7 tip the typical length of the inner cone is about 2 to 2.5 centimeters. With a number 6 or 7 tip, it is preferred to hold the tube rod in the range of from about 1 to 4 centimeters from the tip of the inner cone. If anything, this region of the flame is neutral or slightly carbon-rich and produces carbon-reduction of the metal alloy being welded by providing excess carbon for the chemical reactions between the metal and cermet materials in the hardfacing. By maintaining the tube rod in this preferred location in a longer than usual flame, eta phase and oxide particle formation in the matrix is minimized. In the welding practice according to this embodiment of the invention, the formation of oxide and eta phase particles is insensitive to increases in heat input of the flame, unlike conventional welding practices in which oxide and eta phase particle formation increases with increases in heat input from the flame. In addition, the particle size of the eta phase and oxide particles is greatly refined to less than 30  $\mu\text{m}$ .

The length of the intermediate cone relative to the inner cone, and the neutral condition of the flame are readily adjusted by varying the pressure or flow rate of the oxygen

and acetylene to the torch. This can be accomplished by pressure regulators at the tanks and/or adjustment of the valves on the torch.

A preferred region for the welding rod in a torch flame having 3:1 ratio of cone lengths is between about one and two cm from inner flame cone tip; however it is difficult to maintain the tube rod in this small range during manual welding. Hence, this is a less preferred method of hardfacing. The longer than usual flame with a 4:1 ratio provides a much longer zone within which the welding rod may be placed for achieving a low eta phase and oxide concentration in the matrix of the hardfacing.

The eta phase and oxide content in the matrix may be determined by polishing a cross-section of a tooth with hardfacing with incrementally decreasing sizes of diamond particles from 40  $\mu\text{m}$  to 3  $\mu\text{m}$ . The polished surface is then etched with a reagent of 10 g  $\text{KFe}(\text{CN})_6$ , 10 g KOH and 100 ml water followed by an alcohol rinse. The eta phase and oxide content may be determined using a PGI Imagist image analyzer at 100 $\times$  magnification.

The proportion of carbide in the hardfacing is determined largely by the proportion in the welding "rod" used for applying the hardfacing. Some dilution may occur by alloy steel from the surface of the tooth on the cutter cone. This dilution is not a large contributor since in a typical application of hardfacing to a milled tooth cutter cone for a rock bit, the thickness of hardfacing is in the order 2 mm. The amount of dilution depends to some extent on the technique employed by the welder applying the hardfacing.

The carbide content in the hardfacing can be estimated by metallographic examination of a cross section through the hardfacing. The approximate areas of the carbide and binder phases can be determined. From this, the volume percentages of binder and carbide can be estimated, and in turn the weight percentages. Since use of deoxidizer in the filler of a welding tube is important for producing void free binder phase, the dilution of the carbide filler can be taken into account and the ratio of filler weight to tube weight approximated. A hypothetical tube type welding rod can be projected from a hardfacing deposited on the surface by other techniques.

Thus, for consistency in this specification, the proportion of carbide to alloy steel in the hardfacing is considered on the basis of carbide content in the stick used to melt the hardfacing onto the surface. As pointed out above, the filler of carbide, binder and deoxidizer is 50% to 80% by weight (plus or minus 2%) of the stick and the mild steel tube is 20% to 50% by weight (plus or minus 2%). The filler is about 96% carbide (plus or minus 2%), with a balance of deoxidizer and binder.

The improved hardfacing material is applied to the gage surfaces of the cone and gage row teeth in the same manner previously described for applying the hardfacing mixture to the inner row teeth.

Abrasion tests show that the improved hardfacing materials of this invention exhibit improved wear and fracture resistance over hardfacing materials containing similar proportions of carbide particles but which do not include spherical cast carbide particles. For example, in a hardfacing comprising a carbide component with 70 percent by weight of 16 to 30 mesh crushed cemented carbide and 30 percent by weight of 40 to 80 mesh macrocrystalline carbide, it has been found that by substituting 40 percent by weight of the crushed cemented carbide particles with spherical cast carbide particles in the same size range, loss of hardfacing material due to sliding abrasion wear, chipping, and carbide particle fracture were significantly reduced. It is hypoth-

esized that this improved performance is due to the advantages of both the material and geometry of the spherical cast tungsten carbide particles over the crushed cemented tungsten carbide particles they replace. Cast carbide is inherently harder than cemented carbide and hence is more resistant to abrasion wear. Also, it is believed that the spherical particles are less likely to fracture during actual field use than the crushed particles because although cast tungsten carbide is not inherently tougher than cemented tungsten carbide, the spherical particles lack the sharp edges of the crushed particles which act as stress concentrators and hence are more prone to fracture and breakage.

The improvement in performance of the hardfacing translates directly into increased footage of well drilled and increased rate of penetration, both of which translate directly into lowered costs for the driller.

Other modifications and variations of hardfacing for a rock bit will be apparent to one skilled in the art. It is, therefore, to be understood that within the scope of the appended claims, this invention may be practiced otherwise than as specifically described.

What is claimed is:

1. A rock bit comprising:
  - a body;
  - at least one cutting cone rotatably mounted to an end of the body, wherein the cone includes a gage surface at a heel portion of the cone;
  - a number of teeth on the cone, the teeth including a plurality of inner row teeth and a plurality of gage row teeth located near a heel of each cone, wherein the teeth include a hardfacing comprising:
    - steel in the range of from 20 to 50 percent by weight; and
    - filler in the range of from 50 to 80 percent by weight, the filler comprising in the range of from 10 to 100 percent by weight spherical cast tungsten carbide particles having a particle size between about 16 to 40 mesh.
2. The rock bit of claim 1 comprising filler in the range of from 60 to 75 percent by weight.
3. The rock bit of claim 1 wherein the filler comprises in the range of from 20 to 50 percent by weight spherical cast tungsten carbide particles.
4. The rock bit of claim 1 wherein the filler comprises in the range of from 40 to 100 percent by weight spherical cast tungsten carbide particles.
5. The rock bit of claim 1 wherein the filler comprises in the range of from 10 to 99 percent by weight spherical cast tungsten carbide particles having a particle size between about 16 to 40 mesh, and further comprises tungsten carbide particles selected from the group consisting of spherical cemented, crushed cemented, crushed cast, crushed macrocrystalline, and carburized.
6. The rock bit of claim 5 wherein the filler further comprises spherical cast tungsten carbide particles having a particle size between about 80 to 200 mesh.
7. The rock bit of claim 6 wherein the filler comprises spherical cast tungsten carbide particles having a particle size between about 100 to 200 mesh.
8. The rock bit of claim 5 wherein the filler further comprises macrocrystalline tungsten carbide particles having a particle size between about 40 to 80 mesh.
9. A rock bit as recited in claim 1 wherein the hardfacing comprises in the range of from 10 to 90 percent by weight spherical cast tungsten carbide particles having a particle size between about 16 to 40 mesh, and further comprises ultra-fine tungsten carbide particles in the range of from 10

to 35 percent by weight of the filler material, the particles having a particle size in the range of from about 1 to 50 microns.

10. A rock bit as recited in claim 9 wherein the ultra-fine tungsten carbide particles are selected from the group consisting of carburized, macrocrystalline, and spherical cast.

11. A rock bit as recited in claim 9 wherein the steel in the hardfacing is dispersion strengthened by the ultra-fine tungsten carbide particles.

✓12. A rock bit comprising:

a body;

at least one cutting cone rotatably mounted to an end of the body, wherein the cone includes a gage surface at a heel portion of the cone;

a number of teeth on the cone, the teeth including a plurality of inner row teeth and a plurality of gage row teeth located near a heel of each cone, wherein the teeth include a hardfacing comprising:

steel in the range of from 20 to 50 percent by weight;  
filler in the range of from 50 to 80 percent by weight,  
the filler comprising in the range of from 10 to 100 percent by weight spherical cast tungsten carbide particles having a particle size between about 80 to 200 mesh.

13. The rock bit of claim 12 comprising filler in the range of from 60 to 75 percent by weight.

14. The rock bit of claim 12 wherein the filler comprises in the range of from 20 to 50 percent by weight spherical cast tungsten carbide particles.

15. The rock bit of claim 12 wherein the filler comprises in the range of from 40 to 100 percent by weight spherical cast tungsten carbide particles.

16. The rock bit of claim 12 wherein the filler comprises spherical cast tungsten carbide particles having a particle size between about 100 to 200 mesh.

17. The rock bit of claim 12 wherein the filler comprises in the range of from 10 to 99 percent by weight spherical cast tungsten carbide particles having a particle size between about 80 to 200 mesh, and further comprises spherical cast tungsten carbide particles having a particle size between about 16 to 40 mesh.

18. The rock bit of claim 12 wherein the filler comprises in the range of from 10 to 99 percent by weight spherical cast tungsten carbide particles having a particle size between about 80 to 200 mesh, and further comprises tungsten carbide particles selected from the group including spherical cemented, crushed cemented, crushed cast, and crushed macrocrystalline.

19. The rock bit of claim 18 wherein the filler further comprises macrocrystalline tungsten carbide particles having a particle size between about 40 to 80 mesh.

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20. A rock bit as recited in claim 12 wherein the hard-  
facing comprises in the range of from 10 to 90 percent by  
weight spherical cast tungsten carbide particles having a  
particle size between about 80 to 200 mesh, and further  
comprises ultra-fine tungsten carbide particles in the range  
of from 10 to 35 percent by weight of the filler material, the  
particles having a particle size in the range of from about 1  
to 50 microns.

21. A rock bit as recited in claim 20 wherein the ultra-fine  
tungsten carbide particles are selected from the group con-  
sisting of carburized, macrocrystalline, and spherical cast.

22. A rock bit as recited in claim 20 wherein the steel in  
the hardfacing is dispersion strengthened by the ultra-fine  
tungsten carbide particles.

23. A rock bit comprising:

a body;

at least one cutting cone rotatably mounted to an end of  
the body, wherein the cone includes a gage surface at  
a heel portion of the cone;

a number of teeth on the cone, the teeth including a  
plurality of inner row teeth and a plurality of gage row  
teeth located near a heel of each cone, wherein the teeth  
include a hardfacing comprising:

steel in the range of from 20 to 50 percent by weight;

filler in the range of from 50 to 80 percent by weight, the  
filler comprising in the range of from 10 to 100 percent  
by weight spherical cast tungsten carbide particles  
having a particle size between about 16 to 40 mesh and  
between about 80 to 200 mesh.

24. A rock bit as recited in claim 23 wherein the hard-  
facing comprises in the range of from 10 to 90 percent by  
weight spherical cast tungsten carbide particles having a  
particle size between about 16 and 40 mesh and between  
about 80 to 200 mesh, and further comprises ultra-fine  
tungsten carbide particles in the range of from 10 to 40  
percent by weight of the filler material, the particles having  
a particle size in the range of from about 1 to 50 microns.

25. A rock bit as recited in claim 24 wherein the ultra-fine  
tungsten carbide particles are selected from the group con-  
sisting of carburized, macrocrystalline, and spherical cast.

26. A rock bit as recited in claim 24 wherein the steel in  
the hardfacing is dispersion strengthened by the ultra-fine  
tungsten carbide particles.

27. The rock bit of claim 23 wherein the filler comprises  
spherical cast tungsten carbide particles having a particle  
size between about 100 to 200 mesh.

\* \* \* \* \*

28. A rock bit comprising:

a body;

at least one cutting cone rotatably mounted to an end of the body, wherein the cone includes a gage surface at a heel portion of the cone; and

a number of teeth on the cone, the teeth including a plurality of inner row teeth and a plurality of gage row teeth located near a heel of each cone, wherein the teeth include a hardfacing comprising,

steel, and

filler in the range of from 50 to 80 percent by weight, the filler comprising in the range of from 10 to 100 percent by weight spherical cast tungsten carbide particles having a particle size less than 40 mesh.

29. A rock bit as recited in claim 28 comprising steel in the range of 20 to 50 percent by weight.

30. A rock bit as recited in claim 28 wherein the cast tungsten carbide particles have a particle size between about 16 to less than 40 mesh.

31. A rock bit as recited in claim 28 further comprising spherical tungsten carbide particles having a particle size between greater than 80 to 200 mesh.





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at least one cutting cone rotatably mounted to an end of the body, wherein the cone includes a gage surface at a heel portion of the cone; and

steel, and

37. A rock bit as recited in claim 36 comprising steel in the range of 20 to 50 percent by weight, and wherein the spherical tungsten carbide particles have a particle size between about 16 to less than 40 mesh and between greater than 80 to 200 mesh.

a body;

a number of teeth on the cone, the  
teeth including a plurality of inner row teeth  
and a

plurality of gage row teeth located near a heel  
of each cone, wherein the teeth include a  
hardfacing comprising,

steel, and

filler in the range of from 50  
to 80 percent by weight, the filler  
comprising in the range of from 10 to  
100 percent by weight spherical cast  
tungsten carbide particles having a  
particle size of about 40 mesh.

2007-04-24

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

*This paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" under 37 CFR § 1.10, Mailing Label No. **EL521383879US**.*

For : Reissue of U.S. Patent No. 5,791,422  
Patentee : Dah-Ben Liang, et al.  
Patent No. : 5,791,422  
Patent Issue Date : August 11, 1998  
Title : ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES  
  
Docket No. : 36912/CM/S61

## LETTER TO THE OFFICIAL DRAFTSMAN

Assistant Commissioner for Patents  
Washington, D.C. 20231

Post Office Box 7068  
Pasadena, CA 91109-7068  
August 10, 2000

Commissioner:

Please transfer the drawings from the file of U.S. Patent No. 5,791,422, entitled ROCK BIT WITH HARDFACING MATERIAL INCORPORATING SPHERICAL CAST CARBIDE PARTICLES, issued August 11, 1998, to the accompanying application for Reissue of Letters Patent upon approval of the Reissue Application.

Respectfully submitted,

CHRISTIE PARKER & HALE, LLP

By

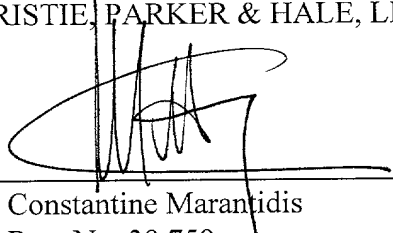
  
Constantine Marantidis  
Reg. No. 39,759  
626/795-9900

Fig. 1

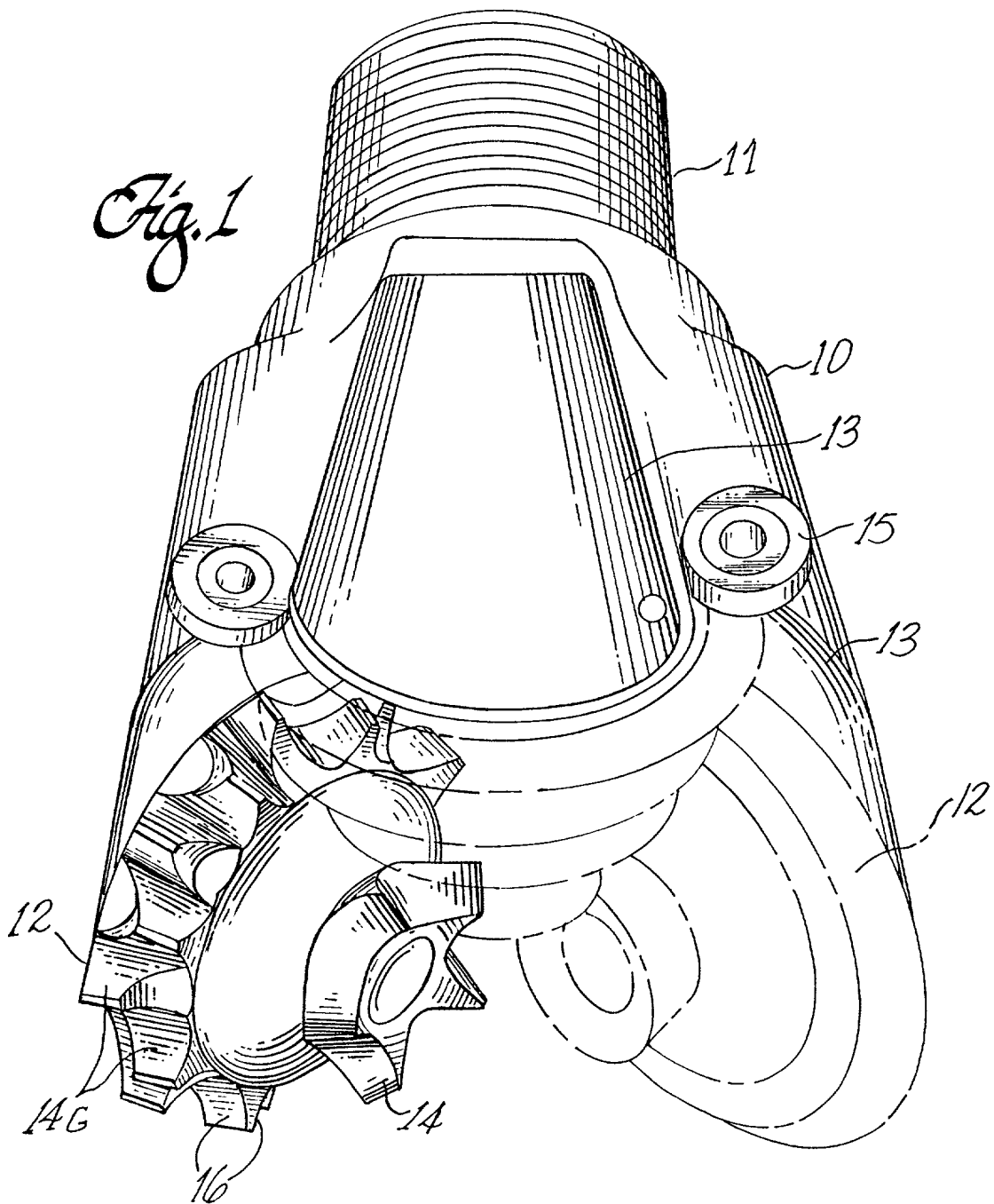


Fig. 2



## PATENT

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

For : Reissue of U.S. Patent No. 5,791,422  
 Patentee : Dah-Ben Liang et al.  
 Patent No. : 5,791,422  
 Patent Issue Date : August 11, 1998  
 Title : ROCK BIT WITH HARDFACING MATERIAL  
 INCORPORATING SPHERICAL CAST  
 CARBIDE PARTICLES  
 Docket No. : 36912/CM/S61

## POWER OF ATTORNEY

Assistant Commissioner for Patents  
 Washington, D.C. 20231

Post Office Box 7068  
 Pasadena, CA 91109-7068

## Commissioner:

The undersigned inventors of the accompanying reissue application for the reissue of Letters Patent No. 5,791,422, granted to them on August 11, 1998, entitled ROCK BIT WITH HARDFACING MATERIAL INCORPORATING SPHERICAL CAST CARBIDE PARTICLES, of which Smith International, Inc., is now sole owner by assignment, and on whose behalf and with whose assent the accompanying application is made, hereby offer to surrender said Letters Patent.

As the named inventors, we hereby appoint:

R. W. Johnston	(17,968)	Edward R. Schwartz	(31,135)	Molly A. Holman	(40,022)
D. Bruce Prout	(20,958)	John D. Carpenter	(34,133)	Lucinda G. Auciello	(42,270)
Hayden A. Carney	(22,653)	David A. Plumley	(37,208)	Norman E. Carte	(30,455)
Richard J. Ward, Jr.	(24,187)	Wesley W. Monroe	(39,778)	Joel A. Kauth	(41,886)
Russell R. Palmer, Jr.	(22,994)	Grant T. Langton	(39,739)	Patrick Y. Ikehara	(42,681)
LeRoy T. Rahn	(20,356)	Constantine Marantidis	(39,759)	Mark Garscia	(31,953)
Richard D. Seibel	(22,134)	John W. Eldredge	(37,613)	Gary J. Nelson	(44,257)
Walter G. Maxwell	(25,355)	Gregory S. Lampert	(35,581)	Raymond R. Tabandeh	(43,945)
William P. Christie	(29,371)	Craig A. Gelfound	(41,032)	Phuong-Quan Hoang	(41,839)
David A. Dillard	(30,831)	Syed A. Hasan	(41,057)	Jun-Young E. Jeon	(43,693)
Thomas J. Daly	(32,213)	Kathleen M. Olster	(42,052)	Kathy Mojibi	(41,409)
Vincent G. Gioia	(19,959)	Daniel M. Cavanagh	(41,661)		

doing business as the law firm CHRISTIE, PARKER & HALE, LLP, telephone 626/795-9900, as principal attorneys with power to appoint associate attorneys, to prosecute this application and

**Docket No. 36912/CM/S61**

any subsequent application based on the disclosure of this application, and to transact all business in the Patent and Trademark Office connected with this application and any subsequent application.

The authority under this Power of Attorney of each person named above shall automatically terminate and be revoked upon such person ceasing to be a member or associate of or of counsel to that law firm.

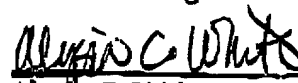
Please address all correspondence to **CHRISTIE, PARKER & HALE, LLP, P.O. Box 7068, Pasadena, California 91109-7068.**

Dated: Aug 9, 2000



Dah-Ben Liang

Dated: Aug. 9, 2000



Alysa C. White

Dated: Aug. 9, 2000



Zhigang Fang

Dated: Aug 9, 2000



Jianen Albert Sue

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## PATENT

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

*This paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" under 37 CFR § 1.10, Mailing Label No. EL521383879US.*

For : Reissue of U.S. Patent No. 5,791,422  
Patentee : Dah-Ben Liang, et al.  
Patent No. : 5,791,422  
Patent Issue Date : August 11, 1998  
Title : ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES  
Docket No. : 36912/CM/S61

## STATEMENT UNDER 37 CFR 3.73(b)

Assistant Commissioner for Patents  
Washington, D.C. 20231

Post Office Box 7068  
Pasadena, CA 91109-7068  
August 8, 2000

## Commissioner:

Smith International, Inc., a Delaware corporation, states that it is the assignee of the entire right, title, and interest in U.S. Patent No. 5,791,422 entitled ROCK BIT WITH HARDFACING MATERIAL INCORPORATING SPHERICAL CAST CARBIDE PARTICLES issued August 11, 1998, by virtue of an assignment to Smith International, Inc., as assignee of Dah-Ben Liang, Alysia C. White, Zhigang Fang, Jiinjen Albert Sue. Title in the name of assignee was recorded on Reel 8607, Frames 0609-0613. A copy of the recorded assignment to Smith International, Inc. from Dah-Ben Liang, Alysia C. White, Zhigang Fang, Jiinjen Albert Sue is enclosed herein.

Respectfully submitted,

By Wesley T. Noah  
Wesley T. Noah, Esq.  
Chief Patent Counsel

Enclosures: Copy of Notice of Recordation of Assignment Document,  
Recordation Form Cover Sheet and Assignment for  
Application No. 08/815,745, filed March 12, 1997

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## PATENT

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

For : Reissue of U.S. Patent No. 5,791,422  
Patentee : Dah Ben Liang, et al.  
Patent No. : 5,791,422  
Patent Issue Date : August 11, 1998  
Title : ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES

Docket No. : 36912/CM/S61

## DECLARATION FOR REISSUE PATENT APPLICATION

Assistant Commissioner for Patents  
Washington, D.C. 20231

Post Office Box 7068  
Pasadena, CA 91109-7068

Commissioner:

As a below named inventor, I hereby declare that I reside at the address listed below, I am a citizen of the United States of America, and I believe I am an original, first and joint inventor of the subject matter described and claimed in U.S. Patent No. 5,791,422 (the "'422 Patent"), issued on August 11, 1998, for which a reissue patent is sought on the invention entitled ROCK BIT WITH HARDFACING MATERIAL INCORPORATING SPHERICAL CAST CARBIDE PARTICLES, the specification of which is attached hereto. The application for the '422 Patent was filed on March 12, 1997, as Application Serial No. 08/815,745 (the "'745 Application").

I acknowledge the duty to disclose information known to me to be material to the examination of this application in accordance with Title 37, Code of Federal Regulations, Section 1.56(a).

I believe that the '422 Patent is partially inoperative because none of the claims in the '422 Patent are directed to a rock bit comprising a cutting cone having a number of teeth which include a hardfacing comprising steel and filler which comprises 10 to 100 percent by weight spherical cast tungsten carbide particles having a particle size less than 40 mesh. The novelty of this aspect of my invention was erroneously overlooked, as I did not appreciate the full scope of the invention being claimed at the time the '745 Application was filed and during its prosecution. My failure to

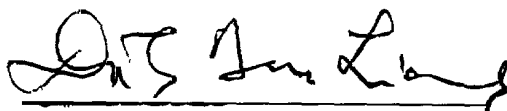
Docket No. 36912/CM/S61

recognize the full scope of the invention being claimed was inadvertent as is evidenced by the fact that although this novel feature was described in the specification of the '745 Application, it was not broadly claimed. As a result of this failure, I claimed less than I had a right to claim in the '422 Patent. This error arose without any deceptive intention on my part.

I hereby state that I have reviewed and understand the content of the above-identified application, including the original claims 1-27 and the added reissue claims 28-38 which are directed to a rock bit comprising a cutting cone having a number of teeth comprising a hardfacing comprising steel and spherical tungsten carbide particles.

I declare further that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, both under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the reissue application or any patent issuing thereon.

Dated: Aug. 9, 2000



Dah-Ben Liang  
27 Rustic View Court  
The Woodlands, Texas 77381

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## PATENT

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

For : Reissue of U.S. Patent No. 5,791,422  
Patentee : Dah Ben Liang, et al.  
Patent No. : 5,791,422  
Patent Issue Date : August 11, 1998  
Title : ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES

Docket No. : 36912/CM/S61

## DECLARATION FOR REISSUE PATENT APPLICATION

Assistant Commissioner for Patents  
Washington, D.C. 20231

Post Office Box 7068  
Pasadena, CA 91109-7068

## Commissioner:

As a below named inventor, I hereby declare that I reside at the address listed below, I am a citizen of the United States of America, and I believe I am an original, first and joint inventor of the subject matter described and claimed in U.S. Patent No. 5,791,422 (the "'422 Patent"), issued on August 11, 1998, for which a reissue patent is sought on the invention entitled ROCK BIT WITH HARDFACING MATERIAL INCORPORATING SPHERICAL CAST CARBIDE PARTICLES, the specification of which is attached hereto. The application for the '422 Patent was filed on March 12, 1997, as Application Serial No. 08/815,745 (the "'745 Application").

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Docket No. 36912/CM/S61

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Dated: Aug 9 2000Alycia C. White

Alycia C. White

4918 Pine Prairie

Kingwood, Texas 77345

Fulshear

4607 Lake Village Drive

77441

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## PATENT

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

For : Reissue of U.S. Patent No. 5,791,422  
Patentee : Dah Ben Liang, et al.  
Patent No. : 5,791,422  
Patent Issue Date : August 11, 1998  
Title : ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES

Docket No. : 36912/CM/S61

## DECLARATION FOR REISSUE PATENT APPLICATION

Assistant Commissioner for Patents  
Washington, D.C. 20231

Post Office Box 7068  
Pasadena, CA 91109-7068

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**Docket No. 36912/CM/S61**

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Dated: Aug. 9, 2000

  
Zhigang Fang  
230 South Crimson Clover Circle  
The Woodlands, Texas 77381

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## PATENT

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

For : Reissue of U.S. Patent No. 5,791,422  
Patentee : Dah Ben Liang, et al.  
Patent No. : 5,791,422  
Patent Issue Date : August 11, 1998  
Title : ROCK BIT WITH HARDFACING MATERIAL  
INCORPORATING SPHERICAL CAST  
CARBIDE PARTICLES

Docket No. : 36912/CM/S61

## DECLARATION FOR REISSUE PATENT APPLICATION

Assistant Commissioner for Patents  
Washington, D.C. 20231

Post Office Box 7068  
Pasadena, CA 91109-7068

## Commissioner:

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Docket No. 36912/CM/S61

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Dated: August 9, 2000

  
Finjen Albert Sue  
22 South Dragonwood Place  
The Woodlands, Texas 77381

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